

Chaos control of unified chaotic system base on tridiagonal matrix stability theory and adaptive hybrid synchronization

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Abstract

This paper presents a new chaos control method to control the unified chaotic system to zero. In order to control a unified chaotic system to zero, the first step is to design a stable system, which stable to zero base on tridiagonal matrix stability theory, the stable system as the master system. The second step is to make the unified chaotic system with controlled as slave system, the third step to make the master system and the slave system synchronization. Different system state apply different adaptive synchronize method to realize synchronization. The adaptive control law and parameter update law are obtained base on Lyapunov stability theory. Numerical simulations are presented to demonstrate the effectiveness of theoretical analysis.

Keywords: chaos control, adaptive hybrid synchronization, tridiagonal structure matrix stability theory

1 Introduction

In 1990, Ott, Grebogi and Yorke presented the OGY method on chaos control [1]. After their pioneering work, chaos control has gained more interest in nonlinear problems and there have been a lot of progress in this field [2-5]. Generally, there are two control ways: feedback control and nonfeedback control. Feedback methods [6-10] are used to stabilize the unstable periodic orbit of chaotic systems by feedback their states. Nonfeedback methods [11, 12] are adopted to suppress chaotic behaviour by apply periodic perturbations to some parameters or variables. With the development of chaos control technology, all kinds of methods are developed.

This paper proposes a new chaos control method to control the unified chaotic system to zero, the new method base on tridiagonal structure matrix stability and hybrid synchronization.

This paper is organized as follows. In the next section, we analyse the tridiagonal structure matrix stability theory and system with tridiagonal structure matrix. In section 3, we introduce the hybrid synchronization theory. In section 4, we make use of tridiagonal matrix stability theory and adaptive hybrid synchronization to control the unified chaotic system to zero. In section 5, some numerical simulations are done to test the effectiveness of theoretical analysis. Finally, some conclusions are drawn in section 6.

2 The theory

2.1 THE TRIDIAGONAL STRUCTURE MATRIX STABILITY THEORY

Lemma 1 [13, 14] If the nonlinear system has the following forms of tridiagonal structure:

$$\dot{X} = \begin{bmatrix} -k_1 & f_1(x) & & & \\ -f_1(x) & -k_2 & & & \\ & \ddots & \ddots & & \\ & & \ddots & f_{n-1}(x) & \\ & & & -f_{n-1}(x) & -k_n \end{bmatrix} X, \text{ where}$$

$X(t) = (x_1, x_2, \dots, x_n)^T \in \mathbb{R}^n$ is state vectors, $f_j(x_i) (j = 1, 2, \dots, n-1, i = 1, 2, 3, \dots, n)$ are function about x_i , $k_i \in \mathbb{R}^+ (i = 1, 2, \dots, n)$, the state vectors x of nonlinear system will be globally asymptotically stabilized to origin.

Proof: A positive definite function is as follows, $V = \frac{1}{2} X^T X$.

$$\text{The derivative of } V, \dot{V} = -\sum_{i=1}^n K_i x_i^2 < 0.$$

Due to V is the Lyapunov function and x will be globally asymptotically stabilized to origin [14].

2.2 SYSTEM WITH TRIDIAGONAL STRUCTURE MATRIX

Due to permanent magnet synchronous motor (PMSM) system has tridiagonal structure, we introduce PMSM system.

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Model of PMSM can be expressed as follows [15],

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} -1 & x_3 & 0 \\ -x_3 & -1 & \gamma \\ 0 & \sigma & -\sigma \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}. \quad (1)$$

The parameters γ and σ ($\sigma > 0$) can decide the system (1) is chaos or not [16]. Fig. 1 show the chaotic character of system (1) with $\gamma=20$ and $\sigma=3$, initial values $x_1(0)=0.1, x_2(0)=0.2, x_3(0)=0.4$. From Figure 1 it can be concluded that system (1) is in chaotic state.

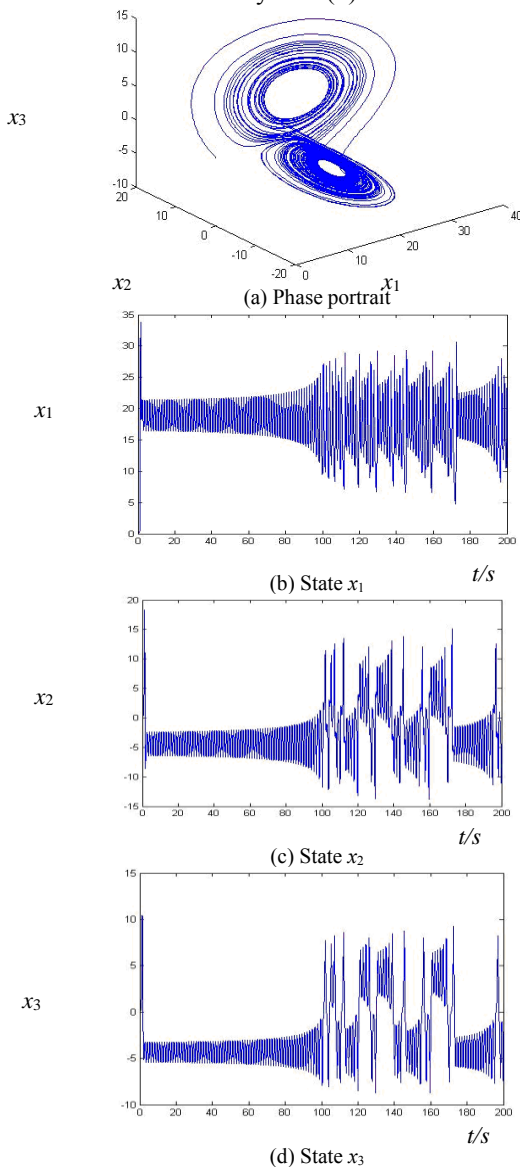


FIGURE 1 the chaotic character of system (1) when $\gamma=20$ and $\sigma=3$

System (1) has tridiagonal structure matrix form when parameters $\gamma = -\sigma$, which can be expressed as follows,

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} -1 & x_3 & 0 \\ -x_3 & -1 & -\sigma \\ 0 & \sigma & -\sigma \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}. \quad (2)$$

Figure 2 shows states changes of system (2) when parameters $\sigma=5$, initial values $x_1(0)=0.1, x_2(0)=0.2, x_3(0)=0.4$. From Figure 2, it can be concluded that system (2) is stabilized to zero.

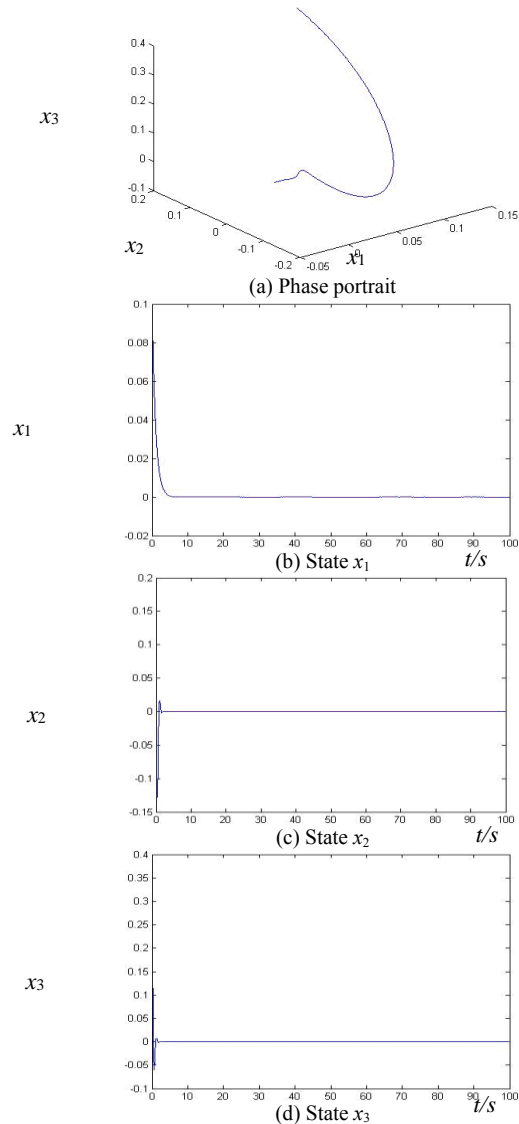


FIGURE 2 Trajectories of the system (2) states when $\sigma=5$

3 Hybrid Synchronization

Consider the following three-dimensional master system (3) and slave system (4),

$$\dot{x} = f(t, x), \quad (3)$$

$$\dot{y} = g(t, y) + u(t, x, y), \quad (4)$$

where $x(t) = (x_1, x_2, x_3)^T \in R^3$ and $y(t) = (y_1, y_2, y_3)^T \in R^3$ are master and slave state vectors respectively, $f: R^3 \rightarrow R^3$ and $g: R^3 \rightarrow R^3$ are continuous nonlinear vector functions and $u(t, x, y) = (u_1, u_2, u_3)^T \in R^3$ is control input for synchronization between master system (3) and slave system (4).

Definition 1. It is said that hybrid synchronization occurs between master system (3) and slave system (4) if satisfy the following conditions:

Define $s(r)$ is a function, where r is state vector.

Satisfy

$$\lim_{t \rightarrow \infty} \|e_1(t) = y_1(t) - s(x_1(t))\| = 0.$$

Define λ is constant and satisfy

$$\lim_{t \rightarrow \infty} \|e_2(t) = y_2(t) - \lambda x_2(t)\| = 0.$$

Define $m(t)$ is a function and satisfy

$$\lim_{t \rightarrow \infty} \|e_3(t) = y_3(t) - m(t)x_3(t)\| = 0.$$

4 Method

The unified chaotic system [17] is expressed as follows,

$$\begin{aligned} \dot{x}_1 &= (25\theta + 10)(x_2 - x_1) \\ \dot{x}_2 &= (28 - 35\theta)x_1 + (29\theta - 1)x_2 - x_1x_3, \\ \dot{x}_3 &= x_1x_2 - \frac{8 + \theta}{3}x_3 \end{aligned} \tag{5}$$

where $\theta \in [0, 1]$. System (5) is chaotic for $\theta \in [0, 1]$.

When $\theta \in [0, 0.8)$, system (5) reduces to the general Lorenz system; when $\theta = 0.8$, it becomes the general Lü

$$\begin{aligned} \dot{e}_1 &= (25\theta + 10)(y_2 - y_1) - \dot{s}_1(x_1)(-x_1 + x_3x_2) + u_1 \\ \dot{e}_2 &= (28 - 35\theta)y_1 + (29\theta - 1)y_2 - y_1y_3 - \lambda(-x_2 - x_3x_1 - 5x_3) + u_2. \\ \dot{e}_3 &= y_1y_2 - \frac{8 + \theta}{3}y_3 - \dot{m}(t)x_3 - m(t)[5(x_2 - x_3)] + u_3 \end{aligned} \tag{9}$$

Here, our goal is to achieve hybrid synchronization between two systems with different initial conditions. For this end, the following control laws are designed:

$$\begin{aligned} u_1 &= -(25\hat{\theta} + 10)(y_2 - y_1) + \dot{s}_1(x_1)(-x_1 + x_2x_3) - k_1e_1 \\ u_2 &= -(28 - 35\hat{\theta})y_1 - (29\hat{\theta} - 1)y_2 + y_1y_3 + \lambda(-x_2 - x_3x_1 - 5x_3) - k_2e_2, \\ u_3 &= -y_1y_2 + \frac{8 + \hat{\theta}}{3}y_3 + \dot{m}(t)x_3 + 5m(t)(x_2 - x_3) - k_3e_3 \end{aligned} \tag{10}$$

where $\tilde{\theta} = \theta - \hat{\theta}$, we define $\hat{\theta}$ as estimate of θ of system (6), $\tilde{\theta}$ is estimate error, $k_i > 0 (i = 1, 2, 3)$.

Substituting Eqs. (10) In Eqs. (9), we obtain

$$\begin{aligned} \dot{e}_1 &= 25\tilde{\theta}(y_2 - y_1) - k_1e_1 \\ \dot{e}_2 &= -35\tilde{\theta}y_1 + 29\tilde{\theta}y_2 - k_2e_2. \\ \dot{e}_3 &= -\frac{\tilde{\theta}}{3}y_3 - k_3e_3 \end{aligned} \tag{11}$$

The parameter update rule for $\hat{\theta}$ is chosen as follows

$$\dot{\hat{\theta}} = \frac{1}{3}e_3y_3 - 25e_1(y_2 - y_1) + e_2(35y_1 - 29y_2). \tag{12}$$

system; and $\theta \in (0.8, 1]$, system (5) is the general Chen system.

We assume that the system (2) with $\sigma = 5$ as master system, system (5) with controlled as the slave system (6) given by,

$$\begin{aligned} \dot{y}_1 &= (25\theta + 10)(y_2 - y_1) + u_1 \\ \dot{y}_2 &= (28 - 35\theta)y_1 + (29\theta - 1)y_2 - y_1y_3 + u_2, \\ \dot{y}_3 &= y_1y_2 - \frac{8 + \theta}{3}y_3 + u_3 \end{aligned} \tag{6}$$

where u_1, u_2, u_3 are the control input.

By the definition of hybrid synchronization, the error is given by

$$\begin{aligned} e_1 &= y_1 - s_1(x_1) \\ e_2 &= y_2 - \lambda x_2 \\ e_3 &= y_3 - m(t)x_3 \end{aligned} \tag{7}$$

The error dynamics system is then given as

$$\begin{aligned} \dot{e}_1 &= \dot{y}_1 - \dot{s}_1(x_1)\dot{x}_1 \\ \dot{e}_2 &= \dot{y}_2 - \lambda\dot{x}_2 \\ \dot{e}_3 &= \dot{y}_3 - \dot{m}(t)x_3 - m(t)\dot{x}_3 \end{aligned} \tag{8}$$

By substituting Eqs. (2) And (6) in the above equation, we obtain

Theorem 1. The system (6) can be stabilized to zero by hybrid synchronization between master system (2) and slave system (6) when choose the control laws (10) and parameter update rule (12).

Proof. Choose the following Lyapunov function

$$V = \frac{1}{2}(e_1^2 + e_2^2 + e_3^2 + \tilde{\theta}^2), \tag{13}$$

where $\tilde{\theta} = \theta - \hat{\theta}$, the time derivative of Eq. (13) along the trajectory of error system is

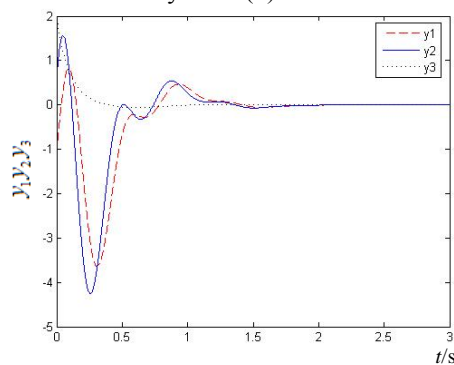
$$\dot{V} = \dot{e}_1e_1 + \dot{e}_2e_2 + \dot{e}_3e_3 + \tilde{\theta}\dot{\tilde{\theta}}, \tag{14}$$

and substitute Eqs. (11) and Eq. (12) in Eq. (14), $\dot{V} = -k_1 e_1^2 - k_2 e_2^2 - k_3 e_3^2$.

Since $\dot{V} < 0$, the master system (2) and the slave system (6) achieve synchronization. The slave system (6) can be stabilized to zero.

5 Numerical simulations

Numerical simulations are presented to demonstrate the effectiveness of the proposed synchronization controller. Fourth-order Runge-Kutta method is used to solve master system (2) and slave system (6) with time step size 0.0001, the parameter of master system (2) are chosen to be $\sigma=5$ so that the master system (2) exhibits stable

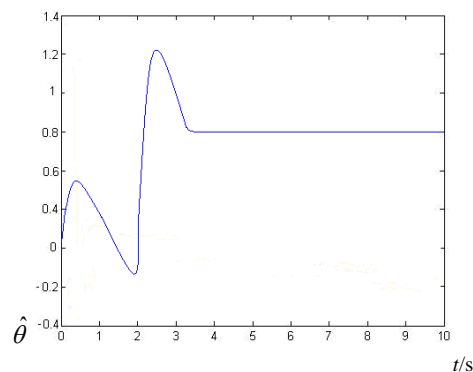


(a) Trajectories of the states y_1, y_2, y_3

behaviour. The initial conditions of the master system (2) as follows, $x_1(0)=0.1, x_2(0)=0.2, x_3(0)=0.3$, and those of the slave system (6) are $y_1(0)=-1, y_2(0)=0.6, y_3(0)=2$.

The estimate parameter of slave system (6) is chosen as $\hat{\theta}=0.1$ real parameter is $\theta=0.8$. Moreover, $s_1(r)=\sin r, s_1(x_1)=\sin x_1, m(t)=\sin t+1, \lambda=30$. The control gains are chosen as $k_1=0.05, k_2=k_3=10$.

The simulations results are illustrated in Fig. 3. From Fig. 3 (a) it can be concluded that system (6) can be stabilized to zero. From Fig. 3 (b) it can be concluded that and estimate parameter value research 0.8.



(b) Parameter identification

FIGURE 3 System (6) control process






6 Conclusions

In this paper, we propose a chaos control method to control the unified chaotic system with uncertain parameter to zero. The first step is to design a stable system, which stabilizes to zero bases on tridiagonal matrix stability theory, the stable system as master system. The second step is to make the unified chaotic

system with controlled as the slave system. The third step is to make the slave system and the master system synchronize. The variables of system apply adaptive function synchronization, adaptive projective synchronization and the adaptive generalized projective synchronization to realize the synchronization of master system and the slave system. Thus, the slave system can be stabilized to zero.

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